# SELECTION AND SCALING OF GROUND MOTION RECORDS FOR SEISMIC ANALYSIS

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# Ground Motion :

- Ground motion is the movement of earths surface from the location of earthquake or explosion.
- Earthquake are usually caused when rock underground the surface of earth suddenly breaks along the fault.

# Selection of Recorded Ground Accelerations for Seismic Design

- Record selection based on earthquake magnitude (M) and distance (R):
- Recorded earthquake can be divided as:

# Magnitude consideration

Large magnitude event  $(6.1 < M \le 6.9)$ 

Medium magnitude event  $(3.4 < M \le 6.1)$ 

Minor magnitude event (M<3.4)

#### **Distance consideration**

Large radius event (40 km< M ≤ 90 km)

Small radius event (12 km< M ≤ 40 km)

### Development of primary record sets

- □ Large magnitude–near fault bin
  - (LMNF;  $6.1 < Mw \le 6.9, 12 \text{ km} \le R$ );
- ☐ Large magnitude—short distance bin

(LMSR; 
$$6.1 < Mw \le 6.9$$
,  $12 \text{ km} < R \le 40 \text{ km}$ );

☐ Large magnitude—long distance bin

$$(LMLR; 6.1 < Mw \le 6.9, 40 \text{ km} < R \le 90 \text{ km});$$

☐ Small magnitude—short distance bin

(SMSR; 
$$5.4 < Mw \le 6.0$$
,  $12 \text{ km} < R \le 40 \text{ km}$ ); and

□ Small magnitude—long distance bin

$$(SMLR; 5.4 < Mw \le 6.0, 40 \text{ km} < R \le 90 \text{ km})$$

### Record selection based on Soil profile

- ☐ It is complementing criteria to both earthquake magnitude and distance.
- □ Shear wave velocity is metric for site classification.
- Based on shear wave velocity soil can be classified as:

A - Rock 
$$760 \text{m/s} \le \text{Vs} 30 \text{m} \le 1500 \text{m/s}$$

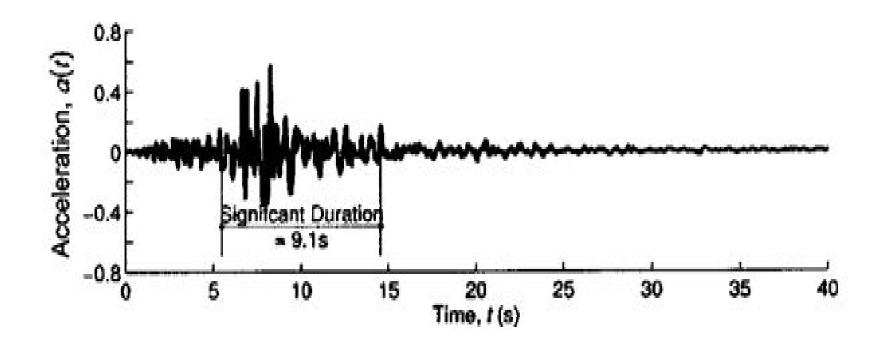
B - Stiff soil 
$$360 \text{m/s} \le \text{Vs} 30 \text{m} \le 760 \text{m/s}$$

C - Soft soil 
$$180 \text{m/s} \le \text{Vs} 30 \text{m} \le 360 \text{m/s}$$

D - Very soft soil 
$$Vs30m \le 180m/s$$

### Record selection based on Strong motion duration

1. Significant duration: Time interval during which 90% of total energy recorded at the station.



# Record selection based on spectral matching

- □ Scaling: spectral matching technique are based on scaling of selected time history in time domain. Multiplying the records with a constant factor to get close to target spectrum at a period(s) of interest.
- Spectral matching in frequency domain: modifying the frequency content to match the target spectrum.
- Spectral matching in time domain: adding the wavelets to match the target design spectrum

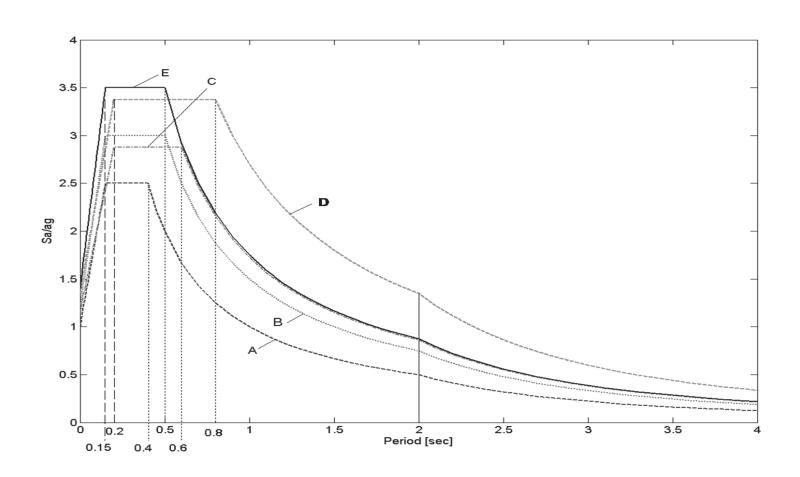
# Seismic code provisions for selection of records

- Seismic codes which prescribe general guidelines to select ground motions are:
- Euro code 8 (Europe)
- ASCE 7 (USA)
- NZS 1170:2004 (New-Zealand)
- GB 50011-2001 (China and Taiwan)

# Ground motion use in Europe

- EC-8 allows the use of any form of accelerograms for structural assessment, i.e. Real, artificial and simulated accelerograms.
- ☐ A minimum of 3 accelerograms.
- ☐ It allow to use 7 accelerograms average values of response quantities.
- ☐ The peak ground acceleration of individual time histories should be greater than codified peak ground acceleration

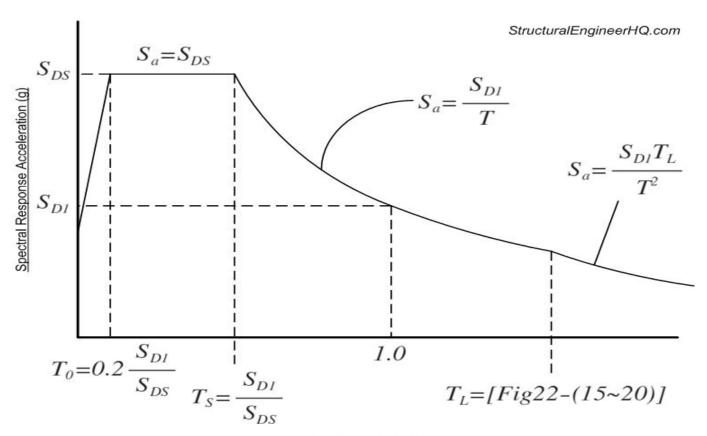
# The spectral shapes given by EC-8



# Ground motion use in United States (ASCE 7)

- □ ASCE-7 provides general guideline for selecting and scaling ground motions use in nonlinear response history analysis of structure.
- ☐ A minimum 3 records are required
- □ The matching of spectrum is performed over the period range of  $0.2T_1$  to  $1.5T_1$
- □ For three dimensional analysis spectrum representing the average of SRSS spectra of all records does not fall below 1.3 times design spectrum

#### Design Response Spectrum



Building Period, T (sec)

#### Ground motion use in New-Zealand

(NZS 1170-2004)

- New-Zealand standard allows to use only actual records for structural assessment.
- □ Currently NZS 1170-2004 recommended that selection of seven records instead of three.
- $\square$  Design spectrum for horizontal loading C(T) is define as:

$$C(T) = C_h(T)ZRN(T,D)$$

where,  $C_h(T)$  = spectral shape factor.

Z = hazard factor

R = return period factor

N = near fault factor

# Ground motion use in China (GB50011-20011) and Taiwan(Code 05)

As per GB50011-20011 minimum 3 records are require.(at least two real and one simulated ground motion records require for analysis)

☐ As per Taiwan standard minimum 3 records are require.

□ Spectral acceleration of each gm should be greater than 0.9 times that of design response spectrum

# Comparison of seismic requirements in different world regions

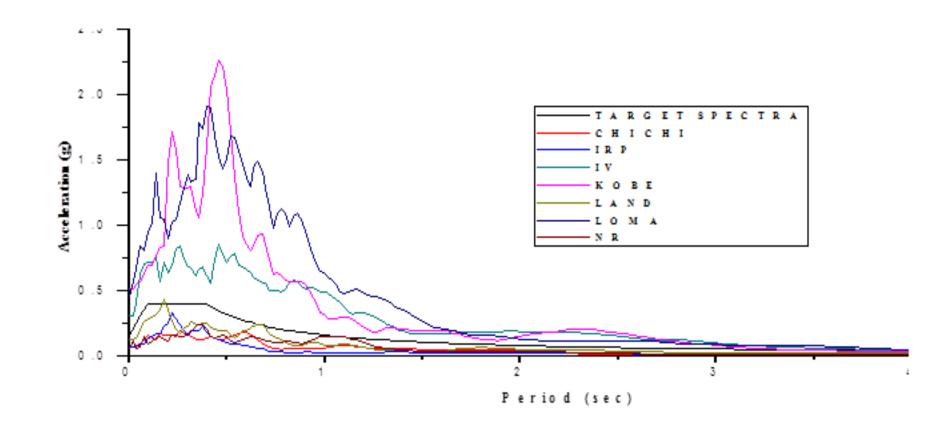
Criteria	Europe	USA	New Zealand	China	Taiwan
Minor Earthquake	95 years			50 years	30 years
Moderate Earthquake	475 years	475 years	500 years	475 years	475 years
Major Earthquake (MCE)		2475 years	2500 years	2000 years	2475 years
Seismic design basis spectrum	475 years	DBE=2/3* MCE	500 years	500 years	475 years
Minimum number of ground motions	3	3	3	3	3
Response of structure	Average response if ≥ 7 records	Average response if ≥ 7 records	Maximum response of 3 records	Average response if ≥ 7 records	Maximum response of 3 records

Criteria	Europe	USA	New Zealand	China	Taiwan
Spectral matching allowed	Yes	Yes	Yes	Yes	Yes
Matching period	0.2T1-2T1	0.2T <sub>1</sub> -1.5T <sub>1</sub>	<b>0.4T</b> 1- <b>1.3T</b> 1		0.2T <sub>1</sub> -1.5T <sub>1</sub>
Matching component	Sa <sub>avg</sub> for all gm > 0.9*target	Saavg for all gm > target	Minimum difference between each gm and target	Sa for each gm > 0.9*target	Sa for each gm > 0.9*target
Artificial records allowed	Yes	Yes	No	Yes	Yes

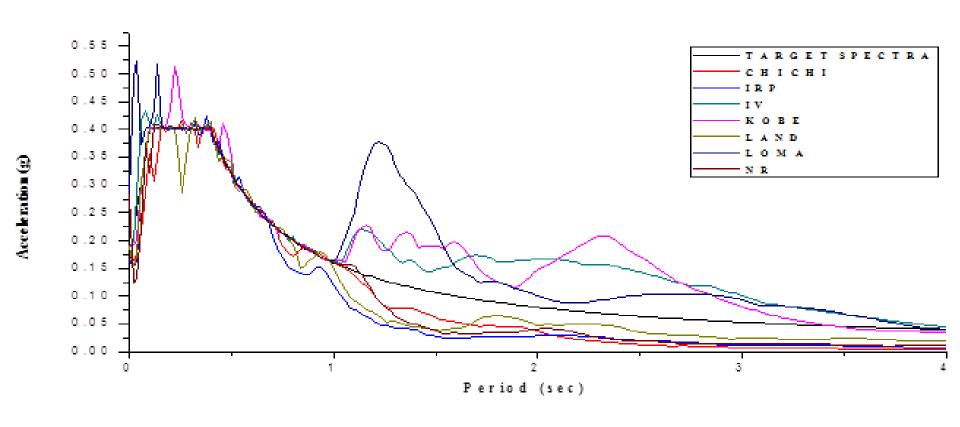
# **Earthquake Excitations**

Earthquake Records Year		Earthquake record description	Recording Direction / Component	Peak ground acceleration
				PGA (g)
Chi-Chi, Taiwan	1999	CHY101	CHICHI/CHY101-W	0.353
Irpina, Italy-01	1980	IRPINIA EQ, STURNO	ITALY/B-STU000	0.071
Imperial Valley, CA	1940	IMPERIAL VALLEY, EL CENTRO ARRAY #9, 180 (USGS STATION 117)	IMPVALL/I-ELC 180	0.313
Kobe, Japan	1995	CUE 99999, NISHI AKASHI	KOBE/NIS000	0.509
Landers, CA	1992	LANDERS, LUCERNE	LANDERS/LCN000	0.785
Loma Prieta, CA	1989	LOMA PRIETA, BRAN (UCSC STATION 13)	LOMAP/BRN000	0.453
Northridge	1994	NORTHRIDGE AFTERSHOCK, ANAVERDE VALLEY - CITY RANCH	NORTHR/ANA180	0.06

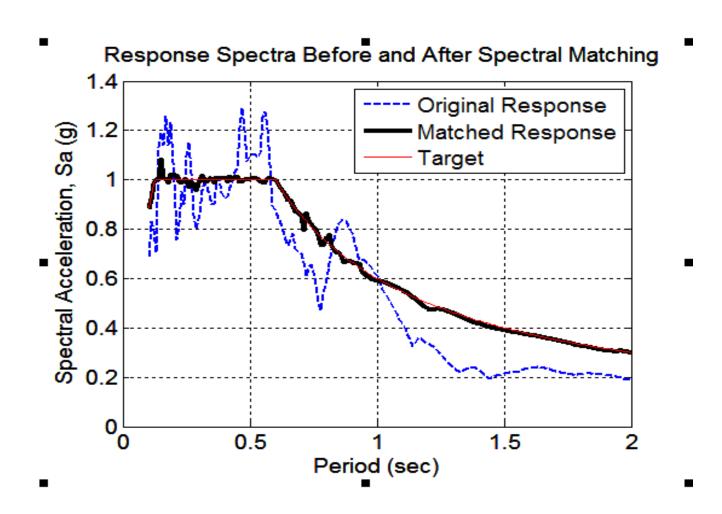
# **Spectral Mapping**



# **Spectral Matching**

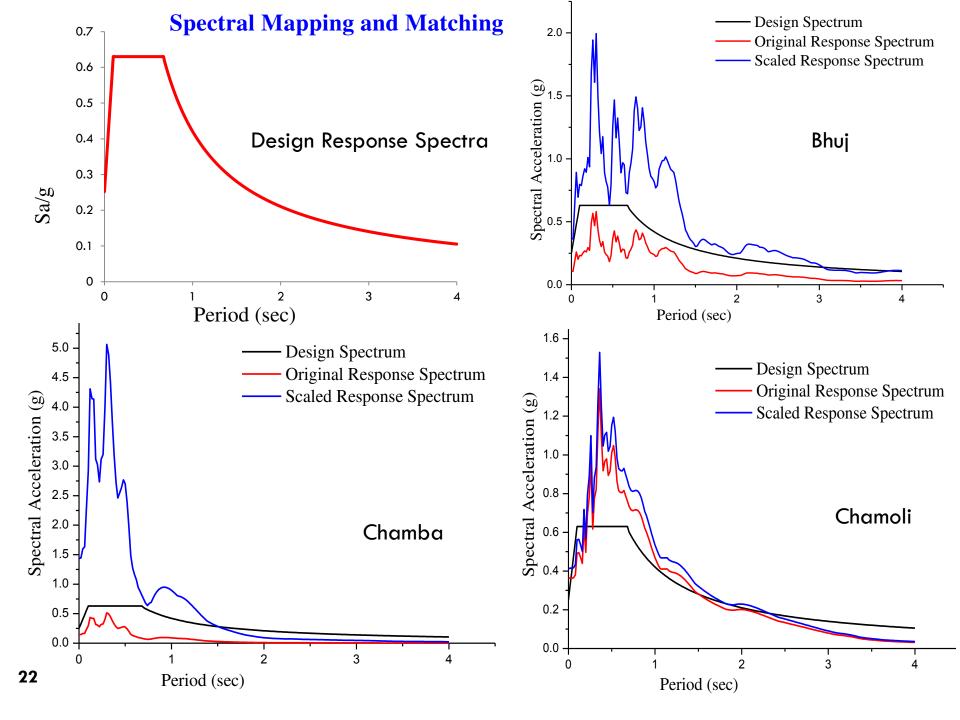


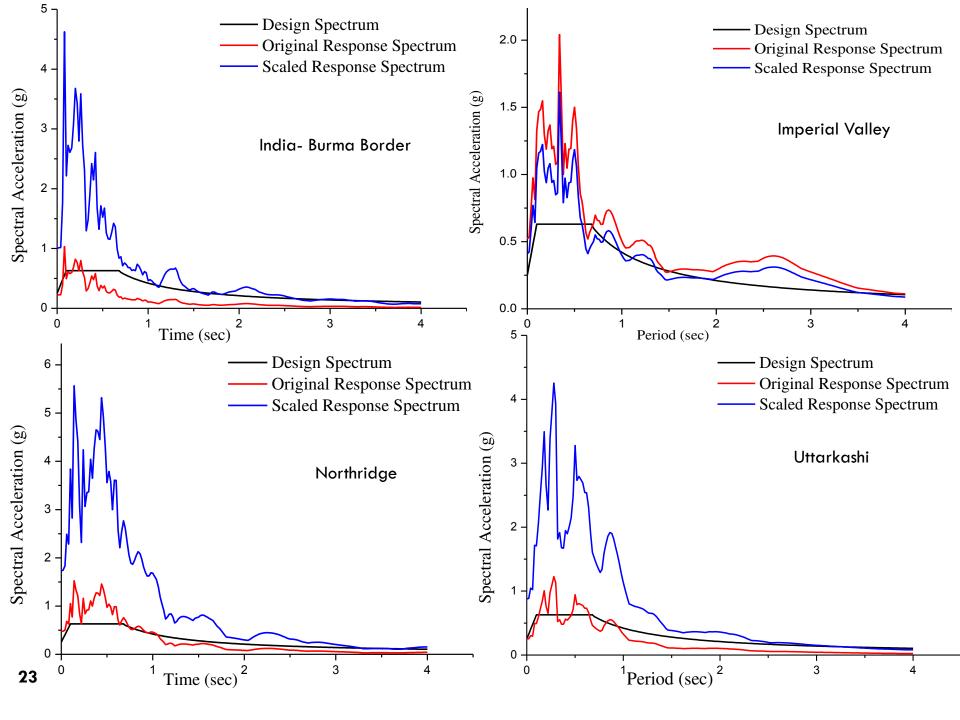
# **Ground motion scaling**

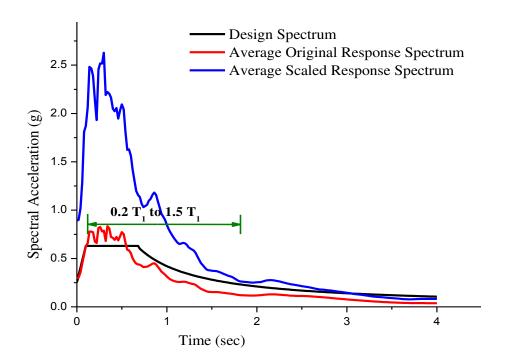


# **Earthquake Records**

Earthquake Records	Year	Earthquake record description	Recording Direction / Component	Peak Ground Acceleration (g)	Scale
Bhuj, India	2001	Ahmedabad, India	N 78 E	0.31	3.43
Chamba, India	1995	Chamba, India	N 00 E	0.47	9.85
Chamoli, India	1999	Gopeshwar, India	N 20 E	0.42	1.14
Ind- Burma Border	1988	Bokajan, India	S 56 E	0.22	4.48
Imperial Valley, CA	1979	USGS 952, El Centro Array 5	S 40 E	0.41	0.79
Northridge	1994	USC, 90091 LA, Saturn St.	N 20 E	0.24	3.65
<u>Uttarkashi</u> , India	1991	Bhatwari, India	N 85 E	0.34	3.47





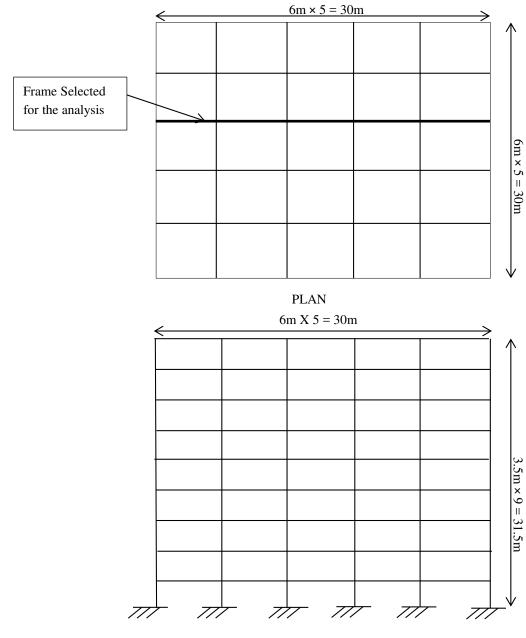


Comparison of average scaled response spectra of all ground motions with design spectrum

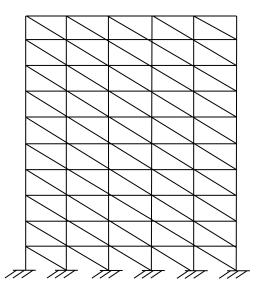
# THANK YOU

# Case Study of Incremental Dynamic Analysis

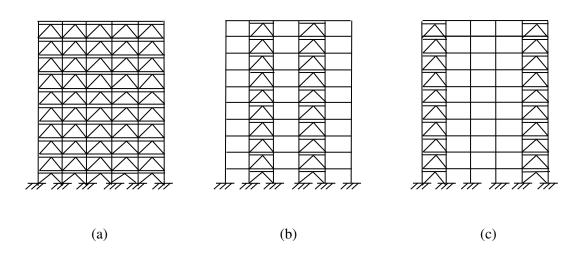




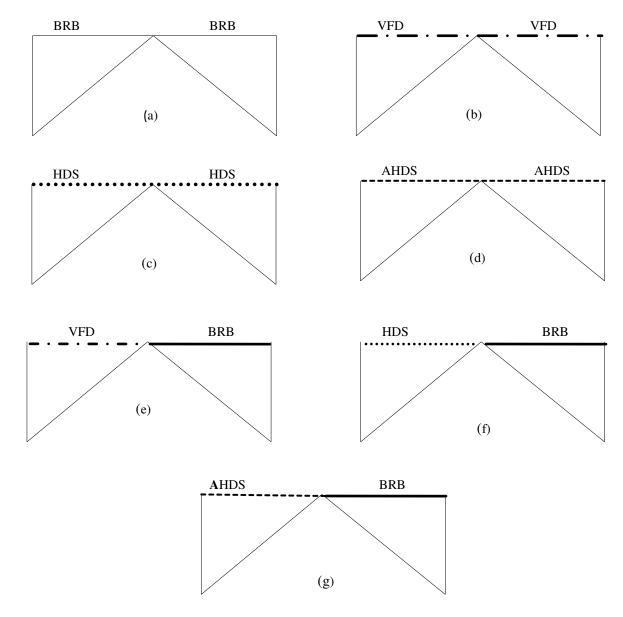
Elevation



Structural frame(with masonry wall)



Structural frame with energy dissipating devices a) Energy Dissipating System in all bays (AO Case) b) Energy Dissipating System in inner - outer bays (IO Case) c) Energy Dissipating System in outer - outer bays (OO Case)



Schematic diagram of MSMRF with (a) BRB on both sides of CB (b) VFD on both sides of CB (c) HDS on both sides of CB (d) AHDS on both sides of CB (e) BRB + VFD on both sides of CB (f) BRB + HDS on both sides of CB (g) BRB + AHDS on both sides of CB

# **Structural Systems**

Sr.	Structural Configuration	Abbreviations
1	Steel Moment Resisting Frame (BARE)	SMRF (Bare)
2	Steel Moment Resisting Frame with masonry infill wall	SMRF (Soft)
3	Modified SMRF with BRB in all bays (BRB AO)	MSMRF + BRB AO
4	Modified SMRF with BRB in Inner – Outer Bays (BRB IO)	MSMRF + BRB IO
5	Modified SMRF with BRB in Outer – Outer Bays (BRB OO)	MSMRF + BRB OO
6	Modified SMRF with VFD in all bays and all stories (VFD AO)	MSMRF + VFD AO
7	Modified SMRF with VFD in inner-outer bays (VFD IO)	MSMRF + VFD IO
8	Modified SMRF with VFD in outer-outer bays (VFD OO)	MSMRF + VFD OO
9	Modified SMRF with HDS in all bays (HDS AO)	MSMRF + HDS AO
10	Modified SMRF with HDS in Inner – Outer Bays (HDS IO)	MSMRF + HDS IO
11	Modified SMRF with HDS in Outer – Outer Bays (HDS OO)	MSMRF + HDS OO
12	Modified SMRF with AHDS in all bays (AHDS AO)	MSMRF + AHDS AO
13	Modified SMRF with AHDS in Inner – Outer Bays (AHDS IO)	MSMRF + AHDS IO
14	Modified SMRF with AHDS in Outer - Outer Bays (AHDS OO)	MSMRF + AHDS OO
15	Modified SMRF with BRB + VFD in all bays (BRB+ VFD) AO	MSMRF + (BRB+VFD) AO
16	Modified SMRF with BRB + VFD in Inner - Outer bays (BRB+VFD) IO	MSMRF + (BRB+VFD) IO
17	Modified SMRF with BRB + VFD in Outer - Outer bays (BRB+VFD) OO	MSMRF + (BRB+VFD) OO
18	Modified SMRF with BRB + HDS in all bays (BRB+HDS) AO	MSMRF + (BRB+HDS) AO
19	Modified SMRF with BRB + HDS in Inner - Outer bays (BRB+HDS) IO	MSMRF + (BRB+HDS) IO
20	Modified SMRF with BRB + HDS in Outer - Outer bays (BRB+HDS) OO	MSMRF + (BRB+HDS) OO
21	Modified SMRF with BRB + AHDS in all bays (BRB+AHDS) AO	MSMRF + (BRB+AHDS) AO
22	Modified SMRF with BRB + AHDS in Inner - Outer bays (BRB+AHDS) IO	MSMRF + (BRB+AHDS) IO
23	Modified SMRF with BRB + AHDS in Outer - Outer bays (BRB+AHDS) OO	MSMRF + (BRB+AHDS) OO

4	W21 × 101		W21 × 101		$W21\times101$		W21 × 101		W21 × 101	
W14×193	W21 × 101	W14 × 211	W21 × 101	W14 × 211	W21×101	W14 × 211	W21× 101	W14×211	W21 × 101	W14 × 193
W14×193	W21 × 101	W14×211	W21 × 101	W14×211	W21 × 101	W14×211	W21 × 101	W14×211	 W21 ×101	W14×193
W14×211	W21 × 147	W14×211	W21 × 147	W14×211	W21 × 147	W14×211	W21 × 147	W14×211	W21 × 147	W14×211
W14 × 233	W21 × 147	W14 × 283	W21 × 147	W14 × 283	W21 × 147	W14 × 283	W21 × 147	W14 × 283	W21 × 147	W14 × 233
W14×233	W24 × 146	W14 × 283	W24 × 146	W14 × 283	W24 × 146	W14 × 283	W24 × 146	W14 × 283	W24 × 146	W14 × 233
W14 × 283	W24 × 146	W14 × 283	W24 × 146	W14 × 283	W24 × 146	W14 × 283	W24 × 146	W14 × 283	W24 × 146	W14 × 283
W14 × 283	W24 × 146	W14 × 342	W24 × 146	W14 × 342	W24 × 146	W14 × 342	W24 × 146	W14 × 342	W24 × 146	W14 × 283
W14 × 283	W24 × 146	W14 × 342	W24 × 146	W14 × 342	W24 × 146	W14 × 342	W24 × 146	W14 × 342	W24 × 146	W14 × 283
W14 × 283	W24 × 146	W14 × 342	W24 × 146	W14 × 342	W24 × 146	W14 × 342	W24 × 146	W14 ×342	W24 × 146	W14 × 283
W14 × 370	7 7,	W14 × 370		W14 × 370	7 7	W14 × 370	<del>/-</del> - <del>/</del>	W14 × 370	T 7,	W14 × 370

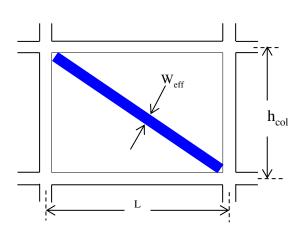
Structural Frame without EDD

	W21 × 73	W21 × 7	73	W21 × 73		W21 × 73		W21 × 73	
W14 × 132	W21 × 73	% W21 × 7	W14 × 176	W21 × 73	W14 × 176	W21 × 73	W14 × 176	W21 × 73	W14 × 132
W14 × 132		921 × 91 × 91 × 91 × 91 × 91 × 91 × 91 ×	14×176	W21 × 93	W14×176	W21 × 93	W14 × 176	W21 × 93	W14 × 132
W14 × 145	W21 × 93	% W21 × 9	3 W14 × 176	W21 × 93	W14×176	W21 × 93	W14×176	W21 × 93	W14 × 145
W14 × 159	W21 × 93	W21 × 9	W14 × 211	W21 × 93	W14 × 211	W21 × 93	W14 × 211	W21 × 93	W14×159
W14 × 159	W24 × 94	W24 × 9	W14×211	W24 × 94	W14 × 211	W24 × 94	W14 × 211	W24 × 94	W14×159
W14×159	W24 × 94	112 × 44 W24 × 94	W14×211	W24 × 94	W14 × 211	W24 × 94	W14 × 211	W24 × 94	W14 × 159
W14 × 233	W24 × 94	% W24 × 9	4 W14 × 283	W24 × 94	W14 × 283	W24 × 94	W14 × 283	W24 × 94	W14 × 233
W14 × 233	W24 × 94	88 × 7 × 7 × 7 × 7 × 7 × 7 × 7 × 7 × 7 ×	W14 × 283	W24 × 94	W14 × 283	W24 × 94	W14 × 283	W24 × 94	W14 × 233
W14 × 233	W24 × 94	82 × 41 × 9 × W24 × 9		W24 × 94	W14 × 283	W24 × 94	W14 × 283	W24 × 94	W14 × 233
W14 × 233	7	W14 × 342	W14 × 342	<del>-</del> -	W14 × 342	<del>7-</del> -	W14 × 342	<del>7</del> -	W14 × 233

**Modified Structural Frame** 

# **Modeling of Wall Strut**





$$W_{eff} = 0.175 \left(\lambda_h h_{col}\right)^{-0.4} r_m$$

where,

$$\lambda_{\rm h} = \sqrt[4]{\frac{E_m t \sin 2\theta}{4E_c I_c h_m}}$$

$$\theta = \tan^{-1} \frac{h_m}{L}$$

 $\lambda_h$  = Coefficient used to determine equivalent width of infill strut

 $h_{col}$  = Column height between center line of beams

h<sub>m</sub> = Height of infill panel

 $E_c$  = Modulus of elasticity of frame material

E<sub>m</sub> = Modulus of elasticity of infill material

I<sub>c</sub> = Moment of Inertia of Column

r<sub>m</sub> = Diagonal Length of Infill Panel

t = Thickness of infill panel and equivalent strut

L = Length of infill panel

# Effective width of wall

Floor	L	$E_{c}$	t	$\theta$	sin2θ	$E_m$	<u>I</u> c	$h_m$	2,	$h_{col}$	$r_m$	$W_{\it eff}$
1 1001	(mm)	(N/mm <sup>2</sup> )	(mm)	(Deg)	SII120	(N/mm <sup>2</sup> )	(mm <sup>4</sup> )	(mm)	∑.h	(mm)	(mm)	(mm)
Floor 0 to 3	6000	200000	230	26.56	0.80	5500	1.42E+09	3000	0.00073	3500	6800	830
Floor 4 to 6	6000	200000	230	27.32	0.82	5500	791000000	3100	0.00085	3500	6800	780
Floor 7 to 9	6000	200000	230	28.07	0.83	5500	266000000	3200	0.00111	3500	6800	700

# **Earthquake Records**

•\$•					
Earthquake Records	Year	Earthquake record description	Recording	Peak Ground	Scale
			Direction /	Acceleration	
			Component	(g)	
Bhuj, India	2001	Ahmedabad, India	N 78 E	0.31	3.43
<u>Chamba</u> , India	1995	<u>Chamba</u> , India	N 00 E	0.47	9.85
Chamoli, India	1999	Gopeshwar, India	N 20 E	0.42	1.14
Ind- Burma Border	1988	<u>Bokajan</u> , India	S 56 E	0.22	4.48
Imperial Valley, CA	1979	USGS 952, El Centro Array 5	S 40 E	0.41	0.79
Northridge	1994	USC, 90091 LA, Saturn St.	N 20 E	0.24	3.65
<u>Uttarkashi</u> , India	1991	Bhatwari, India	N 85 E	0.34	3.47

### **Buckling Restrained Braced Frame**

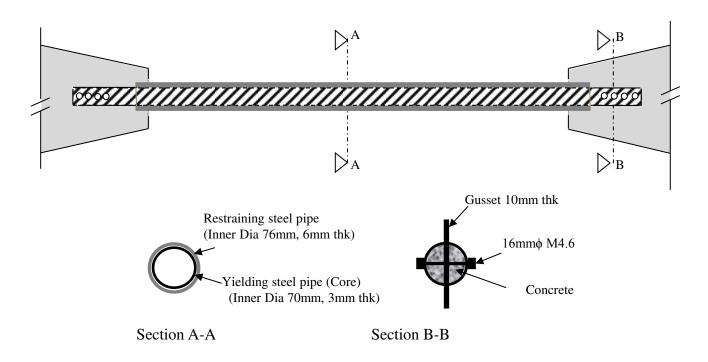
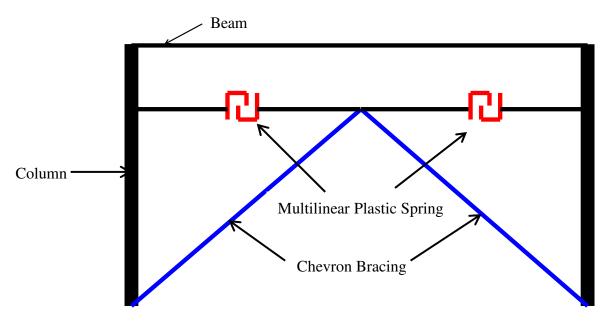


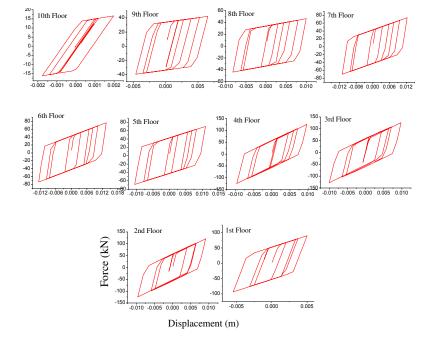
Figure 3.18 Buckling restrained brace

\*\*\* In this research work, BRBs of three variations (Strength wise) are used. Dimensions shown here are of the strongest BRB which is used in bottom four floors.

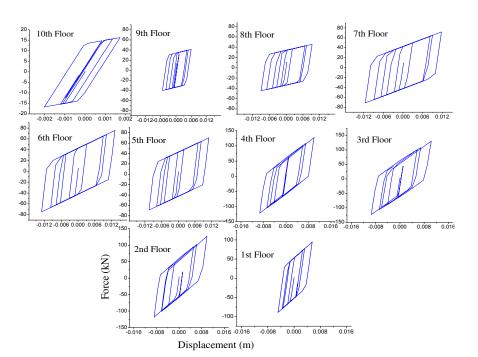
# **Buckling Restrained Braced Frame**



Modeling of BRB placed on both sides of CB



# Device Hysteresis loop for BRB installed in MSMRF (Tension side)

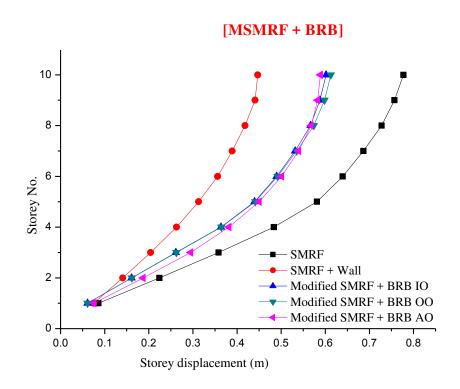


Device Hysteresis loop for BRB installed in MSMRF (Compression side)

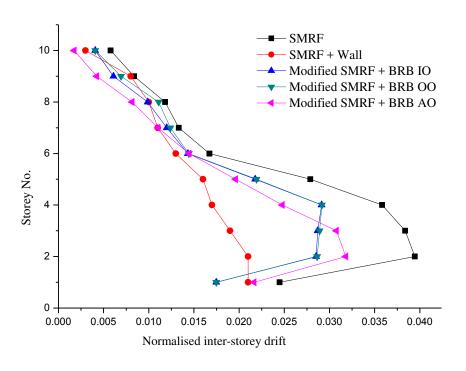
# Dynamic properties of structural configurations with BRB

Sr. No.	Structural configuration	1 <sup>st</sup> mode period (sec)	1 <sup>st</sup> mode frequency (cyc/sec)	1 <sup>st</sup> mode damping ratio	Damping coefficient (kN-s/mm)
1	Steel Moment Resisting Frame (BARE)	1.44	0.69	5.13	N/A
2	Steel Moment Resisting Frame with masonry infill wall	0.81	1.24	6.23	N/A
3	Modified Steel Moment Resisting Frame	1.95	0.51	3.11	N/A
4	Modified SMRF with BRB in All bays (BRB AO)	1.74	0.58	4.31	N/A
5	Modified SMRF with BRB in Inner – Outer Bays (BRB IO)	1.73	0.57	9.12	N/A
6	Modified SMRF with BRB in Outer – Outer Bays (BRB OO)	1.73	0.57	9.03	N/A

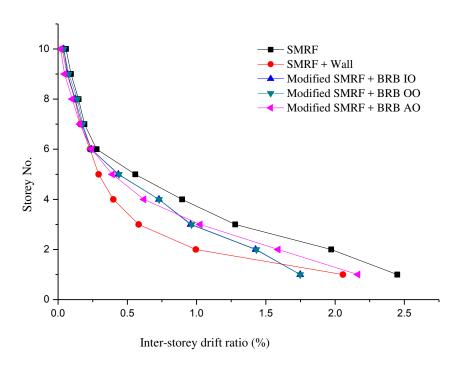
# Storey displacement along the height of the structure



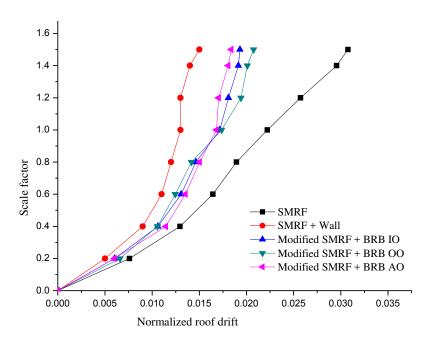
### Inter-storey drift along the height of the structure



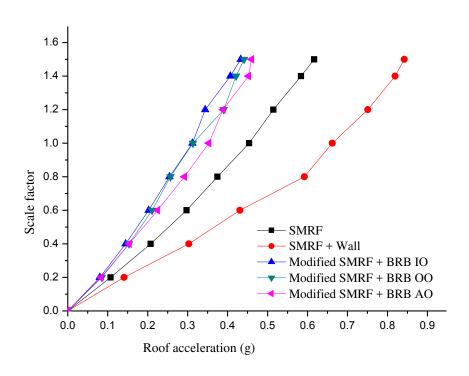
## % Inter-storey drift ratio with respect to scale



# Roof drift with respect to scale factor



## Roof acceleration with respect to scale factor



# Base shear with respect to scale factor

